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## Rolling Process Formulas

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## List of 18 Rolling Process Formulas

## Rolling Process

## Analysis at Entry Region

1) Mean Yield Shear Stress given Pressure on Entry Side
$f \mathrm{fx} \mathrm{S}_{\mathrm{e}}=\frac{\mathrm{P}_{\mathrm{en}} \cdot \frac{\mathrm{h}_{\text {in }}}{\mathrm{h}_{\mathrm{e}}}}{\exp \left(\mu_{\mathrm{rp}} \cdot\left(\mathrm{H}_{\mathrm{in}}-H_{\mathrm{x}}\right)\right)}$
ex $4359.697 \mathrm{~Pa}=\frac{0.0000099 \mathrm{~N} / \mathrm{mm}^{2} \cdot \frac{3.5 \mathrm{~mm}}{0.011 \mathrm{~mm}}}{\exp (0.5 \cdot(3.35-4))}$
2) Pressure Acting on Rolls from Entry Side
$f x$
Open Calculatore
$\mathrm{P}_{\mathrm{en}}=\mathrm{S}_{\mathrm{e}} \cdot \frac{\mathrm{h}_{\mathrm{e}}}{\mathrm{h}_{\mathrm{in}}} \cdot \exp \left(\mu_{\mathrm{rp}} \cdot\left(2 \cdot \sqrt{\frac{\mathrm{R}_{\text {roller }}}{\mathrm{h}_{\mathrm{f}}}} \cdot a \tan \left(\Theta_{\mathrm{r}} \cdot \sqrt{\frac{\mathrm{R}_{\text {roller }}}{\mathrm{h}_{\mathrm{f}}}}\right)-2 \cdot \sqrt{\frac{\mathrm{R}_{\text {roller }}}{\mathrm{h}_{\mathrm{f}}}} \cdot a \tan \left(\alpha_{\mathrm{k}}\right.\right.\right.$
ex
$3.5 \mathrm{E}^{\wedge}-6 \mathrm{~N} / \mathrm{mm}^{2}=4359.69 \mathrm{~Pa} \cdot \frac{0.011 \mathrm{~mm}}{3.5 \mathrm{~mm}} \cdot \exp \left(0.5 \cdot\left(2 \cdot \sqrt{\frac{104 \mathrm{~mm}}{7.5 \mathrm{~mm}}} \cdot a \tan \left(18.5^{\circ} \cdot \sqrt{\frac{104 \mathrm{~mm}}{7.5 \mathrm{~mm}}}\right)-2 \cdot \sqrt{\frac{10}{7 .!}}\right.\right.$
3) Pressure on Rolls given H (Entry Side)
$f \mathrm{f} \mathrm{P}_{\mathrm{en}}=\mathrm{S}_{\mathrm{e}} \cdot \frac{\mathrm{h}_{\mathrm{e}}}{\mathrm{h}_{\mathrm{in}}} \cdot \exp \left(\mu_{\mathrm{rp}} \cdot\left(\mathrm{H}_{\mathrm{in}}-\mathrm{H}_{\mathrm{x}}\right)\right)$
ex $9.9 \mathrm{E}^{\wedge}-6 \mathrm{~N} / \mathrm{mm}^{2}=4359.69 \mathrm{~Pa} \cdot \frac{0.011 \mathrm{~mm}}{3.5 \mathrm{~mm}} \cdot \exp (0.5 \cdot(3.35-4))$
4) Thickness of Stock at given Point on Entry Side
$f \mathbf{f x} \mathrm{~h}_{\mathrm{e}}=\frac{\mathrm{P}_{\mathrm{en}} \cdot \mathrm{h}_{\text {in }}}{\mathrm{S}_{\mathrm{e}} \cdot \exp \left(\mu_{\mathrm{rp}} \cdot\left(\mathrm{H}_{\text {in }}-\mathrm{H}_{\mathrm{x}}\right)\right)}$
ex $0.011 \mathrm{~mm}=\frac{0.0000099 \mathrm{~N} / \mathrm{mm}^{2} \cdot 3.5 \mathrm{~mm}}{4359.69 \mathrm{~Pa} \cdot \exp (0.5 \cdot(3.35-4))}$

## Analysis at Exit Region

5) Mean Yield Shear Stress using Pressure on Exit Side
$f \mathrm{fx} \mathrm{S}_{\mathrm{y}}=\frac{\mathrm{P}_{\text {rolls }} \cdot \mathrm{h}_{\mathrm{ft}}}{\mathrm{h}_{\mathrm{x}} \cdot \exp \left(\mu_{\mathrm{r}} \cdot \mathrm{H}\right)}$
ex $22027.01 \mathrm{~Pa}=\frac{0.000190 \mathrm{~N} / \mathrm{mm}^{2} \cdot 7.3 \mathrm{~mm}}{0.003135 \mathrm{~mm} \cdot \exp (0.6 \cdot 5)}$
6) Pressure Acting on Rolls in Exit Region
$f \mathrm{f} \mathrm{P}_{\mathrm{ex}}=\mathrm{S}_{\mathrm{y}} \cdot \frac{\mathrm{h}_{\mathrm{x}}}{\mathrm{h}_{\mathrm{ft}}} \cdot \exp \left(\mu_{\mathrm{r}} \cdot 2 \cdot \sqrt{\frac{\mathrm{R}_{\mathrm{roll}}}{\mathrm{h}_{\mathrm{ft}}}} \cdot a \tan \left(\Theta_{\mathrm{r}} \cdot \sqrt{\frac{\mathrm{R}_{\mathrm{roll}}}{\mathrm{h}_{\mathrm{ft}}}}\right)\right)$
$\operatorname{ex} 0.000459 \mathrm{~N} / \mathrm{mm}^{2}=22027.01 \mathrm{~Pa} \cdot \frac{0.003135 \mathrm{~mm}}{7.3 \mathrm{~mm}} \cdot \exp \left(0.6 \cdot 2 \cdot \sqrt{\frac{100 \mathrm{~mm}}{7.3 \mathrm{~mm}}} \cdot a \tan \left(18.5^{\circ} \cdot \sqrt{\frac{100 \mathrm{~mm}}{7.3 \mathrm{~mm}}}\right)\right)$
7) Pressure on Rolls given $\mathbf{H}$ (Exit Side)
$f \mathrm{fx} \mathrm{P}_{\text {rolls }}=\mathrm{S}_{\mathrm{y}} \cdot \frac{\mathrm{h}_{\mathrm{x}}}{\mathrm{h}_{\mathrm{ft}}} \cdot \exp \left(\mu_{\mathrm{r}} \cdot \mathrm{H}\right)$
ex $0.00019 \mathrm{~N} / \mathrm{mm}^{2}=22027.01 \mathrm{~Pa} \cdot \frac{0.003135 \mathrm{~mm}}{7.3 \mathrm{~mm}} \cdot \exp (0.6 \cdot 5)$
8) Thickness of Stock at given Point on Exit Side
$f \mathrm{f} \mathrm{h}_{\mathrm{x}}=\frac{\mathrm{P}_{\text {rolls }} \cdot \mathrm{h}_{\mathrm{ft}}}{\mathrm{S}_{\mathrm{y}} \cdot \exp \left(\mu_{\mathrm{r}} \cdot \mathrm{H}\right)}$
ex $0.003135 \mathrm{~mm}=\frac{0.000190 \mathrm{~N} / \mathrm{mm}^{2} \cdot 7.3 \mathrm{~mm}}{22027.01 \mathrm{~Pa} \cdot \exp (0.6 \cdot 5)}$

## Rolling Analysis

9) Angle Subtended by Neutral Point
$f \mathrm{x} \varphi_{\mathrm{n}}=\sqrt{\frac{\mathrm{h}_{\mathrm{fi}}}{\mathrm{R}}} \cdot \tan \left(\frac{\mathrm{H}_{\mathrm{n}}}{2} \cdot \sqrt{\frac{\mathrm{~h}_{\mathrm{fi}}}{\mathrm{R}}}\right)$
ex $5.518163^{\circ}=\sqrt{\frac{7.2 \mathrm{~mm}}{102 \mathrm{~mm}}} \cdot \tan \left(\frac{2.617882}{2} \cdot \sqrt{\frac{7.2 \mathrm{~mm}}{102 \mathrm{~mm}}}\right)$

## 10) Bite Angle

$f \mathrm{x} \alpha_{\mathrm{b}}=a \cos \left(1-\frac{\mathrm{h}}{2 \cdot \mathrm{R}}\right)$
ex $30.03884^{\circ}=a \cos \left(1-\frac{27.4 \mathrm{~mm}}{2 \cdot 102 \mathrm{~mm}}\right)$
11) Factor H at Neutral Point
f. $H_{n}=\frac{H_{i}-\frac{\ln \left(\frac{h_{i}}{h_{\text {fi }}}\right)}{\mu_{f}}}{2}$
$\operatorname{ex} 2.617882=\frac{3.36-\frac{\ln \left(\frac{3.4 \mathrm{~mm}}{7,2 \mathrm{~mm}}\right)}{0.4}}{2}$
12) Factor H used in Rolling Calculations
fx $\mathrm{H}_{\mathrm{r}}=2 \cdot \sqrt{\frac{\mathrm{R}}{\mathrm{h}_{\mathrm{fi}}}} \cdot a \tan \left(\sqrt{\frac{\mathrm{R}}{\mathrm{h}_{\mathrm{fi}}}}\right) \cdot \Theta_{\mathrm{r}}$
ex $3.186783=2 \cdot \sqrt{\frac{102 \mathrm{~mm}}{7.2 \mathrm{~mm}}} \cdot a \tan \left(\sqrt{\frac{102 \mathrm{~mm}}{7.2 \mathrm{~mm}}}\right) \cdot 18.5^{\circ}$
13) Initial Stock Thickness given Pressure on Rolls
fx $\mathrm{h}_{\mathrm{t}}=\frac{\mathrm{S} \cdot \mathrm{h}_{\mathrm{s}} \cdot \exp \left(\mu_{\mathrm{f}} \cdot\left(\mathrm{H}_{\mathrm{i}}-\mathrm{H}_{\mathrm{r}}\right)\right)}{\mathrm{P}}$
ex $1.047159 \mathrm{~mm}=\frac{58730 \mathrm{~Pa} \cdot 0.00313577819561353 \mathrm{~mm} \cdot \exp (0.4 \cdot(3.36-3.18))}{0.000189 \mathrm{~N} / \mathrm{mm}^{2}}$
14) Maximum Reduction in Thickness Possible
fx $\Delta t=\mu_{\mathrm{f}}^{2} \cdot R$
ex $16.32 \mathrm{~mm}=(0.4)^{2} \cdot 102 \mathrm{~mm}$
15) Pressure Considering Rolling Similar to Plane-Strain-Upsetting Process
$f \mathrm{f} \mathrm{P}_{\mathrm{r}}=\mathrm{b} \cdot \frac{2 \cdot \sigma}{\sqrt{3}} \cdot\left(1+\frac{\mu_{\mathrm{sf}} \cdot \mathrm{R} \cdot \frac{\pi}{180} \cdot \alpha_{\mathrm{b}}}{2 \cdot\left(\mathrm{~h}_{\mathrm{i}}+\mathrm{h}_{\mathrm{fi}}\right)}\right) \cdot \mathrm{R} \cdot \frac{\pi}{180} \cdot \alpha_{\mathrm{b}}$
ex $3.3 \mathrm{E}^{\wedge}-5 \mathrm{~N} / \mathrm{mm}^{2}=14.5 \mathrm{~mm} \cdot \frac{2 \cdot 2.1 \mathrm{~N} / \mathrm{mm}^{2}}{\sqrt{3}} \cdot\left(1+\frac{0.41 \cdot 102 \mathrm{~mm} \cdot \frac{\pi}{180} \cdot 30.00^{\circ}}{2 \cdot(3.4 \mathrm{~mm}+7.2 \mathrm{~mm})}\right) \cdot 102 \mathrm{~mm} \cdot \frac{\pi}{180} \cdot 30.00^{\circ}$

## 16) Projected Area

$f \mathbf{f x} A=w \cdot(R \cdot \Delta t)^{0.5}$
ex $1.224 \mathrm{~cm}^{2}=3 \mathrm{~mm} \cdot(102 \mathrm{~mm} \cdot 16.32 \mathrm{~mm})^{0.5}$
17) Projected Length
$f \mathrm{f} L=(\mathrm{R} \cdot \Delta \mathrm{t})^{0.5}$
ex $40.8 \mathrm{~mm}=(102 \mathrm{~mm} \cdot 16.32 \mathrm{~mm})^{0.5}$
18) Total Elongation of Stock
$f x E=\frac{A_{i}}{A_{f}}$
ex $6.666667=\frac{60 \mathrm{~cm}^{2}}{9 \mathrm{~cm}^{2}}$

## Variables Used

- A Projected Area (Square Centimeter)
- $\mathbf{A}_{\mathrm{f}}$ Final Cross Sectional Area (Square Centimeter)
- $\mathbf{A}_{\mathbf{i}}$ Initial Cross Sectional Area (Square Centimeter)
- b Strip Width of Spiral Spring (Millimeter)
- E Total Stock or Workpiece Elongation
- h Height (Millimeter)
- H Factor H at given Point on Workpiece
- $\mathbf{h}_{\mathbf{e}}$ Thickness at Entry (Millimeter)
- $\mathbf{h}_{\mathbf{f}}$ Final Thickness after Rolling (Millimeter)
- $\mathbf{h}_{\mathrm{fi}}$ Thickness after Rolling (Millimeter)
- $\mathbf{h}_{\mathrm{ft}}$ Final Thickness (Millimeter)
- $\mathbf{h}_{\mathbf{i}}$ Thickness before Rolling (Millimeter)
- $\mathbf{H}_{\mathbf{i}}$ Factor H at Entry Point on Workpiece
- $\mathbf{h}_{\mathbf{i n}}$ Initial Thickness (Millimeter)
- $\mathbf{H}_{\text {in }}$ H Factor at Entry Point on Workpiece
- $\mathbf{H}_{\mathbf{n}}$ Factor H at Neutral Point
- $\mathrm{H}_{\mathrm{r}}$ Factor H in Rolling Calculation
- $\mathbf{h}_{\mathbf{s}}$ Thickness at given Point (Millimeter)
- $\mathbf{h}_{\mathbf{t}}$ Initial Stock Thickness (Millimeter)
- $\mathbf{h}_{\mathbf{x}}$ Thickness at the given Point (Millimeter)
- $\mathrm{H}_{\mathbf{x}}$ Factor H at a Point on Workpiece
- L Projected Length (Millimeter)
- P Pressure Acting on Rolls (Newton per Square Millimeter)
- $\mathbf{P e n}_{\text {en }}$ Pressure Acting at Entry (Newton per Square Millimeter)
- $\mathbf{P e x}_{\text {ex }}$ Pressure Acting on Exit (Newton per Square Millimeter)
- $\mathbf{P}_{\mathbf{r}}$ Pressure Acting while Rolling (Newton per Square Millimeter)
- Prolls Pressure on Roller (Newton per Square Millimeter)
- R Roller Radius (Millimeter)
- $\mathbf{R}_{\text {roll }}$ Roll Radius (Millimeter)
- $\mathbf{R}_{\text {roller }}$ Radius of Roller (Millimeter)
- S Mean Yield Shear Stress of Work Material (Pascal)
- $\mathbf{S}_{\mathbf{e}}$ Mean Yield Shear Stress (Pascal)
- $\mathrm{S}_{\mathbf{y}}$ Mean Yield Shear Stress at Exit (Pascal)
- w Width (Millimeter)
- $\boldsymbol{\alpha}_{\mathrm{b}}$ Bite Angle (Degree)
- $\boldsymbol{\alpha}_{\text {bite }}$ Angle of Bite (Degree)
- $\Delta \mathbf{t}$ Change in Thickness (Millimeter)
- $\Theta_{r}$ Angle made by Point Roll Center and Normal (Degree)
- $\mu_{\mathrm{f}}$ Friction Coefficient in Rolling Analysis
- $\mu_{\mathrm{r}}$ Friction Coefficient
- $\mu_{\mathrm{rp}}$ Coefficient of Friction
- $\mu_{\mathbf{s f}}$ Frictional Shear Factor
- $\boldsymbol{\sigma}$ Flow Stress of Work Material (Newton per Square Millimeter)
- $\varphi_{\mathrm{n}}$ Angle subtended at Neutral Point (Degree)


## Constants, Functions, Measurements used

- Constant: pi, 3.14159265358979323846264338327950288

Archimedes' constant

- Function: acos, acos(Number)

The inverse cosine function, is the inverse function of the cosine function. It is the function that takes a ratio as an input and returns the angle whose cosine is equal to that ratio.

- Function: atan, atan(Number)

Inverse tan is used to calculate the angle by applying the tangent ratio of the angle, which is the opposite side divided by the adjacent side of the right triangle.

- Function: cos, $\cos ($ Angle)

Cosine of an angle is the ratio of the side adjacent to the angle to the hypotenuse of the triangle.

- Function: exp, exp(Number)
$n$ an exponential function, the value of the function changes by a constant factor for every unit change in the independent variable.
- Function: $\ln , \ln ($ Number)

The natural logarithm, also known as the logarithm to the base e, is the inverse function of the natural exponential function.

- Function: sqrt, sqrt(Number)

A square root function is a function that takes a non-negative number as an input and returns the square root of the given input number.

- Function: $\boldsymbol{\operatorname { t a n }}, \tan ($ Angle)

The tangent of an angle is a trigonometric ratio of the length of the side opposite an angle to the length of the side adjacent to an angle in a right triangle.

- Measurement: Length in Millimeter (mm)

Length Unit Conversion

- Measurement: Area in Square Centimeter (cm²)

Area Unit Conversion

- Measurement: Pressure in Newton per Square Millimeter ( $\mathrm{N} / \mathrm{mm}^{2}$ ) Pressure Unit Conversion
- Measurement: Angle in Degree ( ${ }^{\circ}$ )

Angle Unit Conversion

- Measurement: Stress in Pascal (Pa) Stress Unit Conversion


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- Composite Materials Formulas
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