



Principal Stress Formulas

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List of 32 Principal Stress Formulas

Principal Stress

Combined Bending and Torsion Condition

1) Angle of Twist in Combined Bending and Torsion

$$heta = rac{rctan\left(rac{T}{M}
ight)}{2}$$

$$extbf{ex} \left[29.99995
ight. ^{\circ} = rac{rctan \left(rac{0.116913 MPa}{67.5 kN^* m}
ight)}{2}
ight.$$

2) Angle of Twist in Combined Bending and Torsional Stress

$$\theta = 0.5 \cdot \arctan \left(2 \cdot rac{T}{\sigma_b}
ight)$$

$$\boxed{\textbf{ex}} 8.995819^\circ = 0.5 \cdot \arctan \bigg(2 \cdot \frac{0.116913 \text{MPa}}{0.72 \text{MPa}} \bigg)$$

3) Bending Moment given Combined Bending and Torsion

$$\mathbf{M} = rac{\mathrm{T}}{ an(2 \cdot heta)}$$

$$= \frac{67.49975 \text{kN*m} = \frac{0.116913 \text{MPa}}{\tan(2 \cdot 30^{\circ})}$$

4) Bending Stress given Combined Bending and Torsional Stress

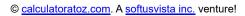
$$\sigma_b = \frac{T}{\frac{\tan(2\cdot\theta)}{2}}$$

5) Torsional Moment when Member is subjected to both Bending and Torsion

$$ag{T} = ext{M} \cdot (an(2 \cdot heta))$$

$$\mathbf{ex} = 0.116913 \text{MPa} = 67.5 \text{kN*m} \cdot (\tan(2 \cdot 30^{\circ}))$$







6) Torsional Stress given Combined Bending and Torsional Stress

$$\mathrm{T} = \left(rac{ an(2\cdot heta)}{2}
ight)\cdot\sigma_{\mathrm{b}}$$

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$$\boxed{\textbf{ex} 0.623538\text{MPa} = \left(\frac{\tan(2\cdot30^\circ)}{2}\right)\cdot0.72\text{MPa}}$$

Complementary Induced Stress

7) Angle of Oblique Plane using Normal Stress when Complementary Shear Stresses Induced 🗹

$$au = rac{a \sin \left(rac{\sigma_{ heta}}{ au}
ight)}{2}$$

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$$oxed{egin{aligned} egin{aligned} oxed{44.4537}^\circ &= rac{a\sin\left(rac{54.99 ext{MPa}}{55 ext{MPa}}
ight)}{2} \end{aligned}}$$

8) Angle of Oblique Plane using Shear Stress when Complementary Shear Stresses Induced 🛂

$$\theta = 0.5 \cdot \arccos \left(rac{ au_{ heta}}{ au}
ight)$$

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$$29.61052^{\circ} = 0.5 \cdot \arccos\left(\frac{28.145 \text{MPa}}{55 \text{MPa}}\right)$$

9) Normal Stress when Complementary Shear Stresses Induced 🗗 fx $\sigma_{\theta} = \tau \cdot \sin(2 \cdot \theta)$

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10) Shear Stress along Oblique Plane when Complementary Shear Stresses Induced

fx
$$\left[au_{ heta} = au \cdot \cos(2 \cdot heta)
ight]$$

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11) Shear Stress due to Effect of Complementary Shear Stresses and Shear Stress in Oblique Plane

$$au = rac{ au_{ heta}}{\cos(2\cdot heta)}$$

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$$au = rac{ au}{\cos(2\cdot heta)}$$

$$\mathbf{ex}$$
 56.29MPa = $\frac{28.145 \text{MPa}}{\cos(2 \cdot 30^{\circ})}$



12) Shear Stress due to Induced Complementary Shear Stresses and Normal Stress on Oblique Plane

$$au = rac{\sigma_{ heta}}{\sin(2\cdot heta)}$$

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Equivalent Bending Moment & Torque

13) Bending Stress of Circular Shaft given Equivalent Bending Moment

$$\sigma_{
m b} = rac{32 \cdot {
m M_e}}{\pi \cdot \left(\Phi^3
ight)}$$

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ex
$$0.724332 \text{MPa} = \frac{32 \cdot 30 \text{kN*m}}{\pi \cdot \left((750 \text{mm})^3 \right)}$$

14) Diameter of Circular Shaft for Equivalent Torque and Maximum Shear Stress

$$\Phi = \left(rac{16\cdot T_{
m e}}{\pi\cdot (au_{
m max})}
ight)^{rac{1}{3}}$$

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ex
$$157.1413$$
mm = $\left(\frac{16 \cdot 32$ kN*m}{\pi \cdot (42MPa) $\right)^{\frac{1}{3}}$

15) Diameter of Circular Shaft given Equivalent Bending Stress

$$\Phi = \left(rac{32\cdot \mathrm{M_e}}{\pi\cdot(\sigma_\mathrm{b})}
ight)^rac{1}{3}$$

Open Calculator

ex
$$751.5011 \text{mm} = \left(\frac{32 \cdot 30 \text{kN*m}}{\pi \cdot (0.72 \text{MPa})}\right)^{\frac{1}{3}}$$

16) Equivalent Bending Moment of Circular Shaft 🗗

$$M_e = rac{\sigma_b}{rac{32}{\pi \cdot (\Phi^3)}}$$

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$$m M_e = rac{\sigma_b}{rac{32}{\pi \cdot (\Phi^3)}}$$

$$= \frac{29.82059 \text{kN*m} = \frac{0.72 \text{MPa}}{\frac{32}{\pi \cdot \left((750 \text{mm})^3 \right)}}$$





17) Equivalent Torque given Maximum Shear Stress

$$T_{
m e}=rac{ au_{
m max}}{16} \ rac{16}{\pi\cdot(\Phi^3)}$$

Open Calculator

$$= \frac{42 MPa}{\frac{16}{\pi \cdot \left((750 mm)^3 \right)}}$$

18) Location of Principal Planes

$$\theta = \left(\left(\left(\frac{1}{2} \right) \cdot a \tan \left(\frac{2 \cdot \tau_{xy}}{\sigma_y - \sigma_x} \right) \right) \right)$$

Open Calculator

$$\boxed{ \mathbf{ex} \left[6.245735^\circ = \left(\left(\left(\frac{1}{2} \right) \cdot a \tan \left(\frac{2 \cdot 7.2 \mathrm{MPa}}{110 \mathrm{MPa} - 45 \mathrm{MPa}} \right) \right) \right) \right] }$$

19) Maximum Shear Stress due to Equivalent Torque

$$au_{
m max} = rac{16 \cdot {
m T_e}}{\pi \cdot \left(\Phi^3
ight)}$$

Open Calculator

Maximum Shear Stress on the Biaxial Loading 🗗

20) Maximum Shear Stress when Member is Subjected to like Principal Stresses 🗹

1

$$au_{ ext{max}} = rac{1}{2} \cdot \left(\sigma_{ ext{y}} - \sigma_{ ext{x}}
ight)$$

Open Calculator 🚰

- 21) Stress along X-Axis when Member is Subjected to like Principal Stresses and Max Shear Stress 🖸

$$\sigma_{
m x} = \sigma_{
m y} - (2 \cdot au_{
m max})$$

Open Calculator 🗗

- $\textbf{ex} \ 26 \text{MPa} = 110 \text{MPa} (2 \cdot 42 \text{MPa})$
- 22) Stress along Y-Axis when Member is Subjected to like Principal Stresses and Max Shear Stress

fx
$$\sigma_{
m y} = 2 \cdot au_{
m max} + \sigma_{
m x}$$

Open Calculator



Stresses in Bi-Axial Loading 🗗

23) Normal Stress Induced in Oblique Plane due to Biaxial Loading

 $\sigma_{\theta} = \left(\frac{1}{2} \cdot \left(\sigma_{x} + \sigma_{y}\right)\right) + \left(\frac{1}{2} \cdot \left(\sigma_{x} - \sigma_{y}\right) \cdot \left(\cos(2 \cdot \theta)\right)\right) + \left(\tau_{xy} \cdot \sin(2 \cdot \theta)\right)$

Open Calculator 🗗

ex

 $\boxed{67.48538 \text{MPa} = \left(\frac{1}{2} \cdot (45 \text{MPa} + 110 \text{MPa})\right) + \left(\frac{1}{2} \cdot (45 \text{MPa} - 110 \text{MPa}) \cdot (\cos(2 \cdot 30^{\circ}))\right) + (7.2 \text{MPa} \cdot \sin(2 \cdot 30^{\circ})) + (7.2 \text{MPa} \cdot \sin(2 \cdot 30^{\circ}))\right)} + (7.2 \text{MPa} \cdot \sin(2 \cdot 30^{\circ})) +$

24) Shear Stress Induced in Oblique Plane due to Biaxial Loading

 $au_{ heta} = -igg(rac{1}{2}\cdotig(\sigma_{ ext{x}} - \sigma_{ ext{y}}ig)\cdot\sin(2\cdot heta)igg) + ig(au_{ ext{xy}}\cdot\cos(2\cdot heta)ig)$

Open Calculator

 $\boxed{\texttt{ex}} \left[31.74583 \text{MPa} = - \left(\frac{1}{2} \cdot \left(45 \text{MPa} - 110 \text{MPa} \right) \cdot \sin(2 \cdot 30^\circ) \right) + \left(7.2 \text{MPa} \cdot \cos(2 \cdot 30^\circ) \right) \right]$

25) Stress along X- Direction with known Shear Stress in Bi-Axial Loading

 $\sigma_{\mathrm{x}} = \sigma_{\mathrm{y}} - \left(rac{ au_{\mathrm{ heta}} \cdot 2}{\sin(2 \cdot heta)}
ight)$

Open Calculator

26) Stress along Y- Direction using Shear Stress in Bi-Axial Loading

 $\sigma_{
m y} = \sigma_{
m x} + \left(rac{ au_{
m heta} \cdot 2}{\sin(2 \cdot heta)}
ight)$

Open Calculator

ex $109.9981\text{MPa} = 45\text{MPa} + \left(\frac{28.145\text{MPa} \cdot 2}{\sin(2 \cdot 30^{\circ})}\right)$

Stresses of Members Subjected to Axial Loading

27) Angle of Oblique Plane using Shear Stress and Axial Load

 $au = rac{ar\sin\left(\left(rac{2\cdot au_0}{\sigma_{
m y}}
ight)
ight)}{2}$

Open Calculator 🗗







28) Angle of Oblique plane when Member Subjected to Axial Loading

$$heta=rac{a\cos\left(rac{\sigma_{_{0}}}{\sigma_{_{y}}}
ight)}{2}$$

$$egin{aligned} \mathbf{ex} \ 30.00301 \ ^{\circ} = rac{a\cos\left(rac{54.99\mathrm{MPa}}{110\mathrm{MPa}}
ight)}{2} \end{aligned}$$

29) Normal Stress when Member Subjected to Axial Load

fx
$$\sigma_{\theta} = \sigma_{y} \cdot \cos(2 \cdot \theta)$$

$$\mathbf{ex} \ 55 \mathrm{MPa} = 110 \mathrm{MPa} \cdot \cos(2 \cdot 30^{\circ})$$

30) Shear Stress when Member Subjected to Axial Load

fx
$$au_{ heta} = 0.5 \cdot \sigma_y \cdot \sin(2 \cdot \theta)$$

31) Stress along Y-direction given Shear Stress in Member subjected to Axial Load

$$\sigma_{
m y} = rac{ au_{
m heta}}{0.5 \cdot \sin(2 \cdot heta)}$$

32) Stress along Y-direction when Member Subjected to Axial Load

$$\sigma_{
m y} = rac{\sigma_{
m heta}}{\cos(2 \cdot heta)}$$

$$\boxed{\textbf{ex} \left[109.98 \text{MPa} = \frac{54.99 \text{MPa}}{\cos(2 \cdot 30^\circ)} \right]}$$



Variables Used

- M Bending Moment (Kilonewton Meter)
- Me Equivalent Bending Moment (Kilonewton Meter)
- T Torsion (Megapascal)
- Te Equivalent Torque (Kilonewton Meter)
- θ Theta (Degree)
- σ_b Bending Stress (Megapascal)
- σ_x Stress along x Direction (Megapascal)
- σ_v Stress along y Direction (Megapascal)
- σ_{θ} Normal Stress on Oblique Plane (Megapascal)
- T Shear Stress (Megapascal)
- Tmax Maximum Shear Stress (Megapascal)
- T_{XV} Shear Stress xy (Megapascal)
- τ_θ Shear Stress on Oblique Plane (Megapascal)
- Φ Diameter of Circular Shaft (Millimeter)





Constants, Functions, Measurements used

- Constant: pi, 3.14159265358979323846264338327950288
 Archimedes' constant
- Function: acos, acos(Number)
 Inverse trigonometric cosine function
- Function: arccos, arccos(Number)
 Inverse trigonometric cosine function
- Function: arctan, arctan(Number)

 Inverse trigonometric tangent function
- Function: arsin, arsin(Number)
 Inverse trigonometric sine function
- Function: asin, asin(Number)
 Inverse trigonometric sine function
- Function: atan, atan(Number)
 Inverse trigonometric tangent function
- Function: cos, cos(Angle)

 Trigonometric cosine function
- Function: ctan, ctan(Angle)

 Trigonometric cotangent function
- Function: sin, sin(Angle)

 Trigonometric sine function
- Function: tan, tan(Angle)

 Trigonometric tangent function
- Measurement: Length in Millimeter (mm)
 Length Unit Conversion
- Measurement: Angle in Degree (°)

 Angle Unit Conversion
- Measurement: Torque in Kilonewton Meter (kN*m)

 Torque Unit Conversion
- Measurement: Moment of Force in Kilonewton Meter (kN*m)

 Moment of Force Unit Conversion
- Measurement: Stress in Megapascal (MPa)
 Stress Unit Conversion





Check other formula lists

- Mohr's Circle of Stresses Formulas
- Beam Moments Formulas
- Bending Stress Formulas
- Combined Axial and Bending Loads Formulas
- Elastic Stability of Columns Formulas
- Principal Stress Formulas
- Slope and Deflection Formulas
- Strain Energy Formulas

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