unitsconverters.com

## Principal Stress Formulas

Bookmark calculatoratoz.com, unitsconverters.com
Widest Coverage of Calculators and Growing - 30,000+ Calculators!
Calculate With a Different Unit for Each Variable - In built Unit Conversion!
Widest Collection of Measurements and Units - 250+ Measurements!

Feel free to SHARE this document with your friends!

Please leave your feedback here...

## List of 32 Principal Stress Formulas

## Principal Stress

## Combined Bending and Torsion Condition

1) Angle of Twist in Combined Bending and Torsion
$\mathrm{fx} \theta=\frac{\arctan \left(\frac{\mathrm{T}}{\mathrm{M}}\right)}{2}$
ex $29.99995^{\circ}=\frac{\arctan \left(\frac{0.116913 \mathrm{MPa}}{67.5 \mathrm{kN} \mathrm{N}^{\mathrm{m}}}\right)}{2}$
2) Angle of Twist in Combined Bending and Torsional Stress
$\theta=0.5 \cdot \arctan \left(2 \cdot \frac{\mathrm{~T}}{\sigma_{\mathrm{b}}}\right)$
$\mathrm{ex} 8.995819^{\circ}=0.5 \cdot \arctan \left(2 \cdot \frac{0.116913 \mathrm{MPa}}{0.72 \mathrm{MPa}}\right)$
3) Bending Moment given Combined Bending and Torsion
$f \mathrm{x} M=\frac{\mathrm{T}}{\tan (2 \cdot \theta)}$
ex $67.49975 \mathrm{kN}^{*} \mathrm{~m}=\frac{0.116913 \mathrm{MPa}}{\tan \left(2 \cdot 30^{\circ}\right)}$
4) Bending Stress given Combined Bending and Torsional Stress
$f \mathbf{f x} \sigma_{\mathrm{b}}=\frac{\mathrm{T}}{\frac{\tan (2 \cdot \theta)}{2}}$
ex $0.135 \mathrm{MPa}=\frac{0.116913 \mathrm{MPa}}{\frac{\tan \left(2 \cdot 30^{\circ}\right)}{2}}$
5) Torsional Moment when Member is subjected to both Bending and Torsion
$f \mathrm{fx}=\mathrm{M} \cdot(\tan (2 \cdot \theta))$
ex $0.116913 \mathrm{MPa}=67.5 \mathrm{kN}^{*} \mathrm{~m} \cdot\left(\tan \left(2 \cdot 30^{\circ}\right)\right)$
6) Torsional Stress given Combined Bending and Torsional Stress
$f_{\mathrm{x}} \mathrm{T}=\left(\frac{\tan (2 \cdot \theta)}{2}\right) \cdot \sigma_{\mathrm{b}}$
ex $0.623538 \mathrm{MPa}=\left(\frac{\tan \left(2 \cdot 30^{\circ}\right)}{2}\right) \cdot 0.72 \mathrm{MPa}$

## Complementary Induced Stress 둔

7) Angle of Oblique Plane using Normal Stress when Complementary Shear Stresses Induced
$f \mathbf{f x} \theta=\frac{a \sin \left(\frac{\sigma_{\theta}}{\tau}\right)}{2}$
ex $44.4537^{\circ}=\frac{a \sin \left(\frac{54.99 \mathrm{MPa}}{55 \mathrm{MPa}}\right)}{2}$
8) Angle of Oblique Plane using Shear Stress when Complementary Shear Stresses Induced
$\mathbf{f x} \theta=0.5 \cdot \arccos \left(\frac{\tau_{\theta}}{\tau}\right)$
ex $29.61052^{\circ}=0.5 \cdot \arccos \left(\frac{28.145 \mathrm{MPa}}{55 \mathrm{MPa}}\right)$
9) Normal Stress when Complementary Shear Stresses Induced
$\mathrm{fx} \sigma_{\theta}=\tau \cdot \sin (2 \cdot \theta)$
ex $47.6314 \mathrm{MPa}=55 \mathrm{MPa} \cdot \sin \left(2 \cdot 30^{\circ}\right)$
10) Shear Stress along Oblique Plane when Complementary Shear Stresses Induced
$f \mathbf{x} \tau_{\theta}=\tau \cdot \cos (2 \cdot \theta)$
ex $27.5 \mathrm{MPa}=55 \mathrm{MPa} \cdot \cos \left(2 \cdot 30^{\circ}\right)$
11) Shear Stress due to Effect of Complementary Shear Stresses and Shear Stress in Oblique Plane $\boxed{\square}$
$\mathrm{fx} \tau=\frac{\tau_{\theta}}{\cos (2 \cdot \theta)}$
ex $56.29 \mathrm{MPa}=\frac{28.145 \mathrm{MPa}}{\cos \left(2 \cdot 30^{\circ}\right)}$
12) Shear Stress due to Induced Complementary Shear Stresses and Normal Stress on Oblique Plane
$f \mathbf{x} \tau=\frac{\sigma_{\theta}}{\sin (2 \cdot \theta)}$
ex $63.49698 \mathrm{MPa}=\frac{54.99 \mathrm{MPa}}{\sin \left(2 \cdot 30^{\circ}\right)}$

## Equivalent Bending Moment \& Torque ©

13) Bending Stress of Circular Shaft given Equivalent Bending Moment
$f \mathrm{x} \sigma_{\mathrm{b}}=\frac{32 \cdot \mathrm{M}_{\mathrm{e}}}{\pi \cdot\left(\Phi^{3}\right)}$
$\mathbf{e x} 0.724332 \mathrm{MPa}=\frac{32 \cdot 30 \mathrm{kN}{ }^{*} \mathrm{~m}}{\pi \cdot\left((750 \mathrm{~mm})^{3}\right)}$
14) Diameter of Circular Shaft for Equivalent Torque and Maximum Shear Stress
$f \mathbf{f x} \Phi\left(\frac{16 \cdot \mathrm{~T}_{\mathrm{e}}}{\pi \cdot\left(\tau_{\max }\right)}\right)^{\frac{1}{3}}$
ex $157.1413 \mathrm{~mm}=\left(\frac{16 \cdot 32 \mathrm{kN}^{*} \mathrm{~m}}{\pi \cdot(42 \mathrm{MPa})}\right)^{\frac{1}{3}}$
15) Diameter of Circular Shaft given Equivalent Bending Stress
$f \mathrm{fx} \Phi=\left(\frac{32 \cdot \mathrm{M}_{\mathrm{e}}}{\pi \cdot\left(\sigma_{\mathrm{b}}\right)}\right)^{\frac{1}{3}}$
ex $751.5011 \mathrm{~mm}=\left(\frac{32 \cdot 30 \mathrm{kN}^{*} \mathrm{~m}}{\pi \cdot(0.72 \mathrm{MPa})}\right)^{\frac{1}{3}}$
16) Equivalent Bending Moment of Circular Shaft
$\mathrm{fx} \mathrm{M}_{\mathrm{e}}=\frac{\sigma_{\mathrm{b}}}{\frac{32}{\pi \cdot\left(\Phi^{3}\right)}}$
ex $29.82059 \mathrm{kN}^{*} \mathrm{~m}=\frac{0.72 \mathrm{MPa}}{\frac{32}{\pi \cdot\left((750 \mathrm{~mm})^{3}\right)}}$
17) Equivalent Torque given Maximum Shear Stress
$\mathrm{T}_{\mathrm{e}}=\frac{\tau_{\max }}{\frac{16}{\pi \cdot\left(\Phi^{3}\right)}}$
ex $3479.068 \mathrm{kN}^{*} \mathrm{~m}=\frac{42 \mathrm{MPa}}{\frac{16}{\pi \cdot\left((750 \mathrm{~mm})^{3}\right)}}$
18) Location of Principal Planes
$\mathrm{fx} \theta=\left(\left(\left(\frac{1}{2}\right) \cdot a \tan \left(\frac{2 \cdot \tau_{\mathrm{xy}}}{\sigma_{\mathrm{y}}-\sigma_{\mathrm{x}}}\right)\right)\right)$
ex $6.245735^{\circ}=\left(\left(\left(\frac{1}{2}\right) \cdot a \tan \left(\frac{2 \cdot 7.2 \mathrm{MPa}}{110 \mathrm{MPa}-45 \mathrm{MPa}}\right)\right)\right)$
19) Maximum Shear Stress due to Equivalent Torque
$\mathrm{fx} \tau_{\max }=\frac{16 \cdot \mathrm{~T}_{\mathrm{e}}}{\pi \cdot\left(\Phi^{3}\right)}$
ex $0.38631 \mathrm{MPa}=\frac{16 \cdot 32 \mathrm{kN}^{*} \mathrm{~m}}{\pi \cdot\left((750 \mathrm{~mm})^{3}\right)}$

## Maximum Shear Stress on the Biaxial Loading

20) Maximum Shear Stress when Member is Subjected to like Principal Stresses
$f \mathrm{x} \tau_{\max }=\frac{1}{2} \cdot\left(\sigma_{\mathrm{y}}-\sigma_{\mathrm{x}}\right)$
ex $32.5 \mathrm{MPa}=\frac{1}{2} \cdot(110 \mathrm{MPa}-45 \mathrm{MPa})$
21) Stress along X-Axis when Member is Subjected to like Principal Stresses and Max Shear Stress
$f \mathbf{f x} \sigma_{\mathrm{x}}=\sigma_{\mathrm{y}}-\left(2 \cdot \tau_{\max }\right)$
ex $26 \mathrm{MPa}=110 \mathrm{MPa}-(2 \cdot 42 \mathrm{MPa})$
22) Stress along Y-Axis when Member is Subjected to like Principal Stresses and Max Shear Stress
$\mathrm{fx} \sigma_{\mathrm{y}}=2 \cdot \tau_{\text {max }}+\sigma_{\mathrm{x}}$
ex $129 \mathrm{MPa}=2 \cdot 42 \mathrm{MPa}+45 \mathrm{MPa}$

## Stresses in Bi-Axial Loading

23) Normal Stress Induced in Oblique Plane due to Biaxial Loading
$\mathrm{fx}_{\mathrm{x}} \sigma_{\theta}=\left(\frac{1}{2} \cdot\left(\sigma_{\mathrm{x}}+\sigma_{\mathrm{y}}\right)\right)+\left(\frac{1}{2} \cdot\left(\sigma_{\mathrm{x}}-\sigma_{\mathrm{y}}\right) \cdot(\cos (2 \cdot \theta))\right)+\left(\tau_{\mathrm{xy}} \cdot \sin (2 \cdot \theta)\right)$
ex
$67.48538 \mathrm{MPa}=\left(\frac{1}{2} \cdot(45 \mathrm{MPa}+110 \mathrm{MPa})\right)+\left(\frac{1}{2} \cdot(45 \mathrm{MPa}-110 \mathrm{MPa}) \cdot\left(\cos \left(2 \cdot 30^{\circ}\right)\right)\right)+(7.2 \mathrm{MPa} \cdot \sin (:$
24) Shear Stress Induced in Oblique Plane due to Biaxial Loading
fx $\tau_{\theta}=-\left(\frac{1}{2} \cdot\left(\sigma_{\mathrm{x}}-\sigma_{\mathrm{y}}\right) \cdot \sin (2 \cdot \theta)\right)+\left(\tau_{\mathrm{xy}} \cdot \cos (2 \cdot \theta)\right)$
ex $31.74583 \mathrm{MPa}=-\left(\frac{1}{2} \cdot(45 \mathrm{MPa}-110 \mathrm{MPa}) \cdot \sin \left(2 \cdot 30^{\circ}\right)\right)+\left(7.2 \mathrm{MPa} \cdot \cos \left(2 \cdot 30^{\circ}\right)\right)$
25) Stress along X- Direction with known Shear Stress in Bi-Axial Loading
$\sigma_{\mathrm{x}}=\sigma_{\mathrm{y}}-\left(\frac{\tau_{\theta} \cdot 2}{\sin (2 \cdot \theta)}\right)$
ex $45.00191 \mathrm{MPa}=110 \mathrm{MPa}-\left(\frac{28.145 \mathrm{MPa} \cdot 2}{\sin \left(2 \cdot 30^{\circ}\right)}\right)$
26) Stress along Y- Direction using Shear Stress in Bi-Axial Loading
$f \mathbf{x} \sigma_{\mathrm{y}}=\sigma_{\mathrm{x}}+\left(\frac{\tau_{\theta} \cdot 2}{\sin (2 \cdot \theta)}\right)$
ex $109.9981 \mathrm{MPa}=45 \mathrm{MPa}+\left(\frac{28.145 \mathrm{MPa} \cdot 2}{\sin \left(2 \cdot 30^{\circ}\right)}\right)$

## Stresses of Members Subjected to Axial Loading

27) Angle of Oblique Plane using Shear Stress and Axial Load
$f \mathbf{f x} \theta=\frac{\operatorname{ar} \sin \left(\left(\frac{2 \cdot \tau_{\theta}}{\sigma_{\mathrm{y}}}\right)\right)}{2}$
ex $15.38948^{\circ}=\frac{a r \sin \left(\left(\frac{2 \cdot 28.145 \mathrm{MPa}}{110 \mathrm{MPa}}\right)\right)}{2}$
28) Angle of Oblique plane when Member Subjected to Axial Loading
$f x \theta=\frac{a \cos \left(\frac{\sigma_{\theta}}{\sigma_{y}}\right)}{2}$
ex $30.00301^{\circ}=\frac{a \cos \left(\frac{54.99 \mathrm{MPa}}{110 \mathrm{MPa}}\right)}{2}$
29) Normal Stress when Member Subjected to Axial Load
$\mathrm{fx} \sigma_{\theta}=\sigma_{\mathrm{y}} \cdot \cos (2 \cdot \theta)$
ex $55 \mathrm{MPa}=110 \mathrm{MPa} \cdot \cos \left(2 \cdot 30^{\circ}\right)$
30) Shear Stress when Member Subjected to Axial Load
$f \mathbf{f} \tau_{\theta}=0.5 \cdot \sigma_{\mathrm{y}} \cdot \sin (2 \cdot \theta)$
ex $47.6314 \mathrm{MPa}=0.5 \cdot 110 \mathrm{MPa} \cdot \sin \left(2 \cdot 30^{\circ}\right)$
31) Stress along Y-direction given Shear Stress in Member subjected to Axial Load
$f \mathrm{x} \sigma_{\mathrm{y}}=\frac{\tau_{\theta}}{0.5 \cdot \sin (2 \cdot \theta)}$
ex $64.99809 \mathrm{MPa}=\frac{28.145 \mathrm{MPa}}{0.5 \cdot \sin \left(2 \cdot 30^{\circ}\right)}$
32) Stress along Y-direction when Member Subjected to Axial Load
$\mathrm{fx} \sigma_{\mathrm{y}}=\frac{\sigma_{\theta}}{\cos (2 \cdot \theta)}$
ex $109.98 \mathrm{MPa}=\frac{54.99 \mathrm{MPa}}{\cos \left(2 \cdot 30^{\circ}\right)}$

## Variables Used

- M Bending Moment (Kilonewton Meter)
- $\mathbf{M}_{\mathbf{e}}$ Equivalent Bending Moment (Kilonewton Meter)
- T Torsion (Megapascal)
- $\mathrm{T}_{\mathrm{e}}$ Equivalent Torque (Kilonewton Meter)
- $\boldsymbol{\theta}$ Theta (Degree)
- $\sigma_{b}$ Bending Stress (Megapascal)
- $\boldsymbol{\sigma}_{\mathbf{x}}$ Stress along x Direction (Megapascal)
- $\sigma_{\mathbf{y}}$ Stress along y Direction (Megapascal)
- $\sigma_{\theta}$ Normal Stress on Oblique Plane (Megapascal)
- t Shear Stress (Megapascal)
- $\mathbf{T}_{\text {max }}$ Maximum Shear Stress (Megapascal)
- $\mathbf{T}_{\mathbf{x y}}$ Shear Stress xy (Megapascal)
- $\boldsymbol{T}_{\boldsymbol{\theta}}$ Shear Stress on Oblique Plane (Megapascal)
- Ф Diameter of Circular Shaft (Millimeter)


## Constants, Functions, Measurements used

- Constant: pi, 3.14159265358979323846264338327950288

Archimedes' constant

- Function: acos, acos(Number)

Inverse trigonometric cosine function

- Function: arccos, arccos(Number)

Inverse trigonometric cosine function

- Function: arctan, arctan(Number)

Inverse trigonometric tangent function

- Function: arsin, arsin(Number) Inverse trigonometric sine function
- Function: asin, asin(Number) Inverse trigonometric sine function
- Function: atan, atan(Number) Inverse trigonometric tangent function
- Function: cos, $\cos ($ Angle)

Trigonometric cosine function

- Function: ctan, ctan(Angle)

Trigonometric cotangent function

- Function: sin, sin(Angle)

Trigonometric sine function

- Function: $\boldsymbol{t a n}, \tan ($ Angle)

Trigonometric tangent function

- Measurement: Length in Millimeter (mm)

Length Unit Conversion

- Measurement: Angle in Degree ( ${ }^{\circ}$ )

Angle Unit Conversion

- Measurement: Torque in Kilonewton Meter (kN*m)

Torque Unit Conversion

- Measurement: Moment of Force in Kilonewton Meter (kN*m)

Moment of Force Unit Conversion

- Measurement: Stress in Megapascal (MPa)

Stress Unit Conversion

## Check other formula lists

- Mohr's Circle of Stresses Formulas
- Beam Moments Formulas
- Bending Stress Formulas
- Combined Axial and Bending Loads Formulas
- Elastic Stability of Columns Formulas
- Principal Stress Formulas
- Slope and Deflection Formulas
- Strain Energy Formulas

Feel free to SHARE this document with your friends!

## PDF Available in

English Spanish French German Russian Italian Portuguese Polish Dutch

